An explicit finite element integration scheme using automatic mesh generation technique for linear convex quadrilaterals over plane regions

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Abstract :

This paper presents an explicit finite element integration scheme to compute the stiffness matrices for plane problems using symbolic mathematics. Stiffness matrices are expressed as double integrals of the products of global derivatives over the all quadrilateral plane region. These matrices can be shown to depend on material and geometric properties matrix and the rational functions with polynomial numerators and linear denominator in bivariates over a 2-square. We have computed the integrals of these rational functions over a 2-square by explicit integration using the symbolic mathematics capabilities of MATLAB. The proposed explicit finite element integration scheme is illustrated by computing the Prandtl stress function values and the torisonal constant for the square cross section by using the four node linear convex quadrilateral finite elements. An automatic all quadrilateral mesh generation techniques which is recently proposed by the authours is also integrated in the appended application programs written in MATLAB.

Key words: Explicit Integration, Gauss Legendre Quadrature, Quadrilateral Function for torsion, Symbolic mathematics, all quadrilateral mesh generation technique.

Element, Prandtl's Stress

1. Introduction :

In recent years, the finite element method (FEM) has emerged as a powerful tool for the approximate solution of differential equations governing diverse physical phenomena. Today, finite element analysis is an integral and major component in many fields of engineering design and manufacturing. Its use in industry and research is extensive, and indeed without it many practical problem in science, engineering and emerging technologies such as nanotechnology, biotechnology, aerospace, chemical. etc would be incapable of solution [1,2,3]. In FEM, various integrals are to be determined numerically in the evaluation of stiffness matrix, mass matrix, body force vector, etc. The algebraic integration needed to derive explicit finite element relations for second order continuum mechanics problems generally defies our analytic skill and in most cases, it appears to be a prohibitive task. Hence, from a practical point of view, numerical integration scheme is not only necessary but very important as well. Among various numerical integration schemes, Gaussian quadrature, which can evaluate exactly the (2n-1)th order polynomial with n Gaussian integration points, is mostly used in view of the accuracy and efficiency of calculation. However, the integrands of global derivative products in stiffness matrix computations of practical applications are not always simple polynomials but rational expressions which the Gaussian quadrature cannot evaluate exactly [7-15]. The integration points have to be increased in order improve the integration accuracy but it is also desirable to make these evaluations by using as few Gaussian points as possible, from the point of view of the computational efficiency. Thus it is important task to strike a proper balance between accuracy and economy in computation. Therefore analytical integration is essential to generate a smaller error as well as to save the computational costs of Gaussian quadrature commonly applied for science, engineering and technical problems. In explicit integration of stiffness matrix, complications arise from two main sources, firstly the large number of integrations that need to be performed and secondly, in methods which use isoparametric elements, the presence of determinant of the Jacobian matrix (we refer this as Jacobian here after) in the denominator of the element matrix integrands. This problem is considered in the recent work [16] for the linear convex quadrilateral proposes a new discretisation method and use of pre computed universal numeric arrays which do not depend on element size and shape. In this method a linear polygon is discretized into a set of linear triangles and then each of these triangles is further discretised into three linear convex quadrilateral elements by joining the centroid to the mid-point of sides. These quadrilateral elements are then mapped into 2-squares ($-1 \le \xi, \eta \le 1$) in the natural space (ξ, n) to obtain the same expression of the Jacobian, namely $c(4+\xi+n)$ where c is some appropriate constant which depends on the geometric data for the triangle.

In the present paper, we propose a similar discretisation method for linear polygon in Cartesian two space (x,y). This discrtisation is carried in two steps, We first discretise the linear polygon into a set of linear triangles in the Cartesian space (x,y) and these linear triangles are then mapped into a standard triangle in a local space (u,v). We further discretise the standard triangles into three linear quadrilaterals by joining the centroid to the midpoints of triangles in (u,v) space which are finally mapped into 2-square in the local (ξ, η) space. We then establish a derivative product relation between the linear convex quadrilaterals in the Cartesian space, (x,y) which are interior to an arbitrary triangle and the linear quadrilaterals in the local space (u,v) interior to the standard triangle. In this procedure, all computations in the local space (u,v) for product of global derivative integrals are free from geometric properties and hence they are pure numbers. We then propose a numerical scheme to integrate the products of global derivatives. We have shown that the matrix product of global derivative integrals is expressible as matrix triple product comprising of geometric properties matrices and the product of local derivative integrals matrix. We have obtained explicit integration of the product of local derivatives which is now possible by use of symbolic integration commands available in leading mathematical softwares MATLAB, MAPLE, MATHEMATIKA etc. In this paper, we have used the MATLAB symbolic mathematics to compute the integrals of the products of local derivatives in (u, v) space. The proposed explicit integration scheme is shown as a useful technique in the formation of element stiffness matrices for second order boundary problems governed by partial differential equations.

2. Explicit form of the Jacobian For a linear Convex Quadrilateral:

Let us first consider an arbitrary four noded linear convex quadrilateral element in the global Cartesian system (u, v) as in Fig 1a. which is mapped in to a 2-square in the local parametric system (ξ , η) as in Fig 1b. is given by



 $\begin{pmatrix} u \\ v \end{pmatrix} = \sum_{k=1}^{4} \begin{pmatrix} u_k \\ v_k \end{pmatrix} N_k(\xi, \eta)$ ----- (1) Where (u_k, v_k) , (k=1,2,3,4) are the vertices of the quadrilateral element in (u, v) plane and $N_k(\xi, \eta)$ denotes the shape function of node k, and they are expressed as [1-3] $N_{k}(\xi,\eta) = \frac{1}{4} \left(1 + \xi_{k}\xi\right) \left(1 + \eta_{k}\eta\right)$ ----- (2a) Where { $(\xi_k, \eta_k), k = 1, 2, 3, 4$ } = {(-1, -1), (1, -1), (1, 1), (-1, 1)} (2b) From the Eq.(1) and Eq.(2), we have Similarly $\frac{\partial v}{\partial \xi} = \frac{1}{4} \left[\left(-v_1 + v_2 + v_3 - v_4 \right) + \left(v_1 - v_2 + v_3 - v_4 \right) \eta \right] \\ \frac{\partial v}{\partial \eta} = \frac{1}{4} \left[\left(-v_1 - v_2 + v_3 + v_4 \right) + \left(v_1 - v_2 + v_3 - v_4 \right) \xi \right]$ ----- (3c) ----- (3d) Hence the Jacobian, J can be expressed as [1, 2, 3] $J = \frac{\partial(u, v)}{\partial(\xi \eta)} = \frac{\partial u}{\partial \xi} \frac{\partial v}{\partial \eta} - \frac{\partial u}{\partial \eta} \frac{\partial v}{\partial \xi} = \alpha + \beta \xi + \gamma \eta$ ----- (4a) Where $\alpha = \frac{1}{8} [(u_4 - u_2)(v_1 - v_3) + (u_3 - u_1)(v_4 - v_2)]$ $\beta = \frac{1}{8} [(u_4 - u_3)(v_2 - v_1) + (u_1 - u_2)(v_4 - v_3)]$ $\gamma = \frac{1}{8} [(u_4 - u_1)(v_2 - v_3) + (u_3 - u_2)(v_4 - v_1)]$ ----- (4b)

3. Global Derivatives:

If N_i denotes the basis functions of node i of any order of the element e, then the chain rule of differentiation from Eq.(1) we can write the global derivative as in [1, 2, 3]



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Where $\frac{\partial u}{\partial \xi}$, $\frac{\partial u}{\partial \eta}$, $\frac{\partial v}{\partial \xi}$ and $\frac{\partial v}{\partial \eta}$ are defined as in Eqs.(3a)–(3d) while J is defined in Eq.(4), (i, j = 1,2,3,..., nde), nde = the number of nodes per element

4. Discretisation of an arbitrary triangle:

A linear convex polygon in the (x, y) plane can be always discretised into a finite number of linear triangles. However, we would like to study a particular discretization of these triangles further into linear convex quadrilaterals. This is stated in the following Lemma [6].

Lemma 1. Let Δ PQR be an arbitrary triangle with the vertices $P(x_p, y_p)$, $Q(x_q, y_q)$ and $R(x_r, y_r)$ and S, T, U be the midpoints of sides PQ, QR and RP respectively and let Z be its centroid. We can obtain three linear convex quadrilaterals ZTRU, ZUPS and ZSQT from triangle Δ PQR as shown in Fig2. If we map each of these quadrilaterals into 2-squares in which the nodes are oriented in counter clockwise from Z then Jacobian J for each element e is given by

 $J = J^{e} = \frac{1}{48} \Delta pqr (4 + \xi + \eta), \qquad e = 1,2,3 \qquad ------(6)$ Where Δpqr is the area of the triangle ΔPQR $2\Delta pqr = \begin{vmatrix} 1 & x_{p} & y_{p} \\ 1 & x_{q} & y_{q} \\ 1 & x_{r} & y_{r} \end{vmatrix} = [(x_{p} - x_{r})(y_{q} - y_{r}) - (x_{q} - x_{r})(y_{p} - y_{r})] \qquad ------(7)$



Proof : Proof is straight forward and given in [16]

We now prove a new result in the form of following Lemma :

Lemma 2. Let Δ PQR be an arbitrary triangle with the vertices $P(x_p, y_p)$, $Q(x_q, y_q)$ and $R(x_r, y_r)$, let S, T, U be the midpoints of sides PQ, QR, and RP and let Z be the centroid of Δ PQR, Then we obtain three quadrilaterals Q₁, Q₂, Q₃ spanning the vertices $\langle ZUPS \rangle$, $\langle ZSQT \rangle$ and $\langle ZTRU \rangle$. these quadrilaterals can be mapped into the quadrilateral spanning vertices GECF with G(1/3, 1/3), E(0, ½), C(0, 0) and F(1/2, 0) of the right isosceles triangle Δ ABC with spanning vertices A(1, 0), B(0, 1) and C(0, 0) in the (u, v) space as shown in Fig 3a and Fig 3b



map the arbitrary triangle Δ PQR into a right isosceles triangle A(1, 0), B(0, 1) and C(0, 0) in the uv-plane We can now verify that quadrilateral Q₁ spanned by vertices Z($\frac{x_p+x_q+x_r}{3}$, $\frac{y_p+y_q+y_r}{3}$), U($\frac{x_r+x_p}{2}$, $\frac{y_r+y_q}{2}$), P(x_p, y_p) ,S($\frac{x_p+x_q}{2}$, $\frac{y_p+y_q}{2}$) in xy- plane is mapped into the quadrilateral spanning the vertices G(1/3, 1/3), E(0, ¹/₂), C(0, 0) and F(1/2, 0) by use of the transformation given in Eq.(8),

Similarly, we see that the quadrilateral Q_2 spanned by vertices Z,S,Q,T is mapped into the quadrilateral spanned by vertices G(1/3, 1/3), $E(0, \frac{1}{2})$, C(0, 0) and $F(\frac{1}{2}, 0)$ by use of the transformation of Eq.(9), Finally the quadrilateral Q_3 in the xy- plane is mapped into the quadrilateral GECF in uv- plane by use of the linear transformation of Eq.(10), This completes the proof.

We have shown in the present section that an arbitrary triangle can be discretised into three linear convex quadrilaterals. Further, each of these quadrilaterals can be mapped into a unique quadrilateral in uv-plane spanned by vertices $(1/3, 1/3), (0, \frac{1}{2}), (0, 0)$ and $(\frac{1}{2}, 0)$.

5. Composite Integration over an arbitrary triangle:

We shall now establish a composite integration formula for an arbitrary triangular region Δ PQR shown in Fig 2a or Fig 3a We have for an arbitrary smooth function $\phi(x, y)$

$$= \iint_{\widehat{Q}} \sum_{e=1}^{3} \left[\varphi \left(x^{(e)}(u, v), y^{(e)}(u, v) \right) \frac{\partial \left(x^{(e)}(u, v), y^{(e)}(u, v) \right)}{\partial (u, v)} \right] dudv$$

= $(2 \Delta_{pqr}) \iint_{\widehat{Q}} \left\{ \sum_{e=1}^{3} \left[\varphi \left(x^{(e)}(u, v), y^{(e)}(u, v) \right) \right] \right\} dudv$ -------(13)

Where $(x^{(e)}(u,v), y^{(e)}(u,v)), e = 1,2,3)$ are the transformations of Eqs.(8)–(10) and \hat{Q} is the quadrilateral in uv- plane spanned by vertices G(1/3, 1/3), E(0, 1/3), E(0, 1/3), E(0, 1/3)) are the transformations of Eqs.(8)–(10) and \hat{Q} is the quadrilateral in uv- plane spanned by vertices G(1/3, 1/3), E(0, 1/3)) are the transformations of Eqs.(8)–(10) and \hat{Q} is the quadrilateral in uv- plane spanned by vertices G(1/3, 1/3), E(0, 1/3)) are the transformations of Eqs.(8)–(10) and \hat{Q} is the quadrilateral in uv-plane spanned by vertices G(1/3, 1/3)). $\frac{1}{2}$, C(0, 0) and F(1/2,0), and Δ_{pqr} is the area of triangle Δ PQR, Now using the transformations defined in Eqs.(1)–(2) we obtain

$$\Pi_{\Delta PQR} = (2 \Delta_{pqr}) \iint_{\widehat{Q}} \{ \sum_{e=1}^{3} [\Phi(x^{(e)}(u, v), y^{(e)}(u, v)) \frac{\partial(u, v)}{\partial(\xi, \eta)} \} d\xi d\eta$$
 ------ (14)
In Eq.(14) we have used the transformation

$$u(\xi, \eta) = \frac{1}{3} N_1(\xi, \eta) + \frac{1}{2} N_4(\xi, \eta)$$

$$v(\xi, \eta) = \frac{1}{3} N_1(\xi, \eta) + \frac{1}{2} N_2(\xi, \eta)$$

$$(15)$$
to map, the quadrilateral \widehat{Q} into a 2 – square in ξn – plane

to map the quadrilateral Q into a 2 – square in $\xi\eta$ – plane. We can now obtain from Eqs.(14)–(15)

II $_{\Delta PQR} = (2 \Delta_{pqr}) \int_{-1}^{1} \int_{-1}^{1} \left[\sum_{e=1}^{3} \left(\frac{4+\xi+\eta}{96} \right) \phi(x^{(e)}(u,v), y^{(e)}(u,v)) \right] d\xi d\eta$ ------ (16) We can evaluate Eq.(16) either analytically or numerically depending on the form of the integrand.

Using Numerical Integration;

Where,

 $u_{i,j}^{(N)} = u(\xi_i^{(N)}, \eta_j^{(N)})$ and $v_{i,j}^{(N)} = v(\xi_i^{(N)}, \eta_j^{(N)})$ ------ (18) and $(W_i^{(N)}, \xi_i^{(N)})$, $(W_j^{(N)}, \xi_j^{(N)})$ are the weight coefficients and sampling points of Nth order Gauss Legendre $u_{i,j}^{(N)} = u(\xi_i^{(N)}, \ \eta_j^{(N)}) \ \text{ and } \ v_{i,j}^{(N)} = v(\xi_i^{(N)}, \ \eta_j^{(N)})$ Quadrature rules.

The above composite rule is applied to numerical Integration over polygonal domains using convex quadrangulation and Gauss Legendre Quadrature Rules[27].

6. Global Derivative Integrals:

If $N_i^{(e)}$ denotes the basis function for node i of element e , then by chain rule of partial differentiation

We note that to transform $Q_e(e = 1,2,3)$ of ΔPQR in Cartesian space (x,y) into \widehat{Q} , the quadrilateral spanned by vertices (1/3,1/3), (0,1/2), (0,0) and (1/2,0) in uv-plane we must use the earlier transformations.

$$\begin{pmatrix} x \\ y \end{pmatrix} = \begin{pmatrix} x_p \\ y_p \end{pmatrix} + \begin{pmatrix} x_q - x_p \\ y_q - y_p \end{pmatrix} u + \begin{pmatrix} x_r - x_p \\ y_r - y_p \end{pmatrix} v \text{ for } Q_1 \text{ in } \Delta PQR \qquad (8)$$

$$\begin{pmatrix} x \\ y \end{pmatrix} = \begin{pmatrix} x_q \\ y_q \end{pmatrix} + \begin{pmatrix} x_r - x_q \\ y_r - y_q \end{pmatrix} u + \begin{pmatrix} x_p - x_q \\ y_p - y_q \end{pmatrix} v \text{ for } Q_2 \text{ in } \Delta PQR \qquad (9)$$

$$\begin{pmatrix} x \\ y \end{pmatrix} = \begin{pmatrix} x_r \\ y_r \end{pmatrix} + \begin{pmatrix} x_p - x_r \\ y_p - y_r \end{pmatrix} u + \begin{pmatrix} x_q - x_r \\ y_q - y_r \end{pmatrix} v \text{ for } Q_3 \text{ in } \Delta PQR \qquad (10)$$
and the above transformations viz Eqs.(8)-(10) are of the form

$$\begin{pmatrix} \mathbf{x} \\ \mathbf{y} \end{pmatrix} = \begin{pmatrix} \mathbf{x}_c \\ \mathbf{y}_c \end{pmatrix} + \begin{pmatrix} \mathbf{x}_a - \mathbf{x}_c \\ \mathbf{y}_a - \mathbf{y}_c \end{pmatrix} \mathbf{u} + \begin{pmatrix} \mathbf{x}_b - \mathbf{x}_c \\ \mathbf{y}_b - \mathbf{y}_c \end{pmatrix} \mathbf{v}$$
(20)

which can map an arbitrary triangle $\triangle ABC$, A(x_a,y_a), B(x_b,y_b), C(x_c,y_c) in xy – plane into a right isosceles triangle in the uv – plane Hence, we have

 $\begin{pmatrix} u \\ v \end{pmatrix} = \begin{pmatrix} (x_a - x_c) & (x_b - x_c) \\ (y_a - y_c) & (y_b - y_c) \end{pmatrix}^{-1} \begin{pmatrix} x - x_c \\ y - y_c \end{pmatrix}$ This gives ----- (21) $u = (\alpha_a + \beta_a x + \gamma_a y)/(2 \Delta_{abc})$ $v = (\alpha_b + \beta_b x + \gamma_b y)/(2 \Delta_{abc})$ ----- (22) $\begin{aligned} & (x_{b} + p_{b}x + \gamma_{b}y)/(2 \Delta_{abc}) \\ & (x_{a} = (x_{b}y_{c} - x_{c}y_{b}) , \qquad & (x_{b} = (x_{c}y_{a} - x_{a}y_{c}) , \\ & \beta_{a} = (y_{b} - y_{c}) , \qquad & \beta_{b} = (y_{c} - y_{a}) , \\ & \gamma_{a} = (x_{c} - x_{b}) , \qquad & \gamma_{b} = (x_{a} - x_{c}) , \\ & \frac{\partial(x,y)}{\partial(u,v)} = 2\Delta_{abc} = \begin{vmatrix} 1 & x_{a} & y_{a} \\ 1 & x_{b} & y_{b} \\ 1 & x_{c} & y_{c} \end{vmatrix} = 2 * \text{ area of the triangle } \Delta ABC \end{aligned}$

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$$= (\gamma_{b}\beta_{a} - \gamma_{a}\beta_{b})$$
Hence from Eq.(19) and Eq.(22), we obtain
$$\left(\frac{\partial N_{i}^{e}}{\partial x} \right)^{2} = \left(\frac{\beta_{a}}{2\Delta_{abc}} & \frac{\beta_{b}}{2\Delta_{abc}} \\ \frac{\gamma_{a}}{2\Delta_{abc}} & \frac{\gamma_{b}}{2\Delta_{abc}} \\ \frac{\gamma_{a}}{2\Delta_{abc}} & \gamma_{b}^{*} \right) \left(\frac{\partial N_{i}^{e}}{\partial x_{i}^{0}} \\ \frac{\partial N_{i}^{e}}{\partial y} \\ \end{array} \right)$$

$$= \left(\beta_{a}^{*} & \beta_{b}^{*} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) \left(\frac{\partial N_{i}^{e}}{\partial x_{i}^{0}} \\ \frac{\partial N_{i}^{e}}{\partial x} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) \left(\frac{\partial N_{i}^{e}}{\partial x_{i}^{0}} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) \left(\frac{\partial N_{i}^{e}}{\partial x_{i}^{0}} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) \\ \gamma_{b}^{*} = \frac{\beta_{b}}{(2\Delta_{abc})} , \qquad \gamma_{b}^{*} = \frac{\beta_{b}}{(2\Delta_{abc})}$$

$$\gamma_{a}^{*} = \frac{\beta_{a}}{(2\Delta_{abc})} , \qquad \gamma_{b}^{*} = \frac{\beta_{b}}{(2\Delta_{abc})}$$
Letting,
$$D_{x,y}^{1,e} = \left(\frac{\partial N_{i}^{e}}{\partial x} \\ \frac{\partial N_{i}^{e}}{\partial y} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) , \qquad P = \left(\beta_{a}^{*} & \beta_{b}^{*} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) , \qquad D_{u,v}^{1,e} = \left(\frac{\partial N_{i}^{e}}{\partial u} \\ \frac{\partial N_{i}^{e}}{\partial y} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \right) , \qquad D_{u,v}^{1,e} = \left(\frac{\partial N_{i}^{e}}{\partial u} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \\ \gamma_{a}^{*} & \gamma_{b}^{*} \\ \gamma_$$

We now define the submatrices of global derivative integrals in (x,y) and (u,v) space associated with the nodes i and j as ;

where, we have already defined the quadrilaterals Q_e (e=1,2,3) in (x,y) space and \hat{Q} in (u,v) space in Fig 3a-b. From Eqs.(28)-(31), we obtain the following relations connecting the submatrices $S^{i,j,e}$ and $K^{i,j,e}$. We now obtain the submatrices $S^{i,j,e}$ and $K^{i,j,e}$ in an explicit form from Eqs.(28a)- (28b) as

$$S^{i,j,e} = \iint_{Q_e} G_{x,y}^{i,j,e} dx dy = \begin{pmatrix} \iint_{Q_e} \frac{\partial N_i^e}{\partial x} \frac{\partial N_j^e}{\partial x} dx dy & \iint_{Q_e} \frac{\partial N_i^e}{\partial x} \frac{\partial N_j^e}{\partial y} dx dy \\ \iint_{Q_e} \frac{\partial N_i^e}{\partial y} \frac{\partial N_j^e}{\partial x} dx dy & \iint_{Q_e} \frac{\partial N_i^e}{\partial y} \frac{\partial N_j^e}{\partial y} dx dy \end{pmatrix}$$

= $\begin{pmatrix} S_{2i-1,2j-1}^e & S_{2i-2j}^e \\ S_{2i,2j-1}^e & S_{2i,2j}^e \end{pmatrix}$ (say) -----(32)
and in similar manner

$$K^{i,j,e} = \iint_{\widehat{Q}} G_{u,v}^{i,j,e} du dv = \begin{pmatrix} \iint_{\widehat{Q}} \frac{\partial N_{i}^{e} \partial N_{j}^{e}}{\partial u} du dv & \iint_{\widehat{Q}} \frac{\partial N_{i}^{e} \partial N_{j}^{e}}{\partial u} du dv \\ \iint_{\widehat{Q}} \frac{\partial N_{i}^{e} \partial N_{j}^{e}}{\partial v} du dv & \iint_{\widehat{Q}} \frac{\partial N_{i}^{e} \partial N_{j}^{e}}{\partial v} du dv \end{pmatrix} \\ = \begin{pmatrix} K_{2i-1,2j-1}^{e} & K_{2i-1,2j}^{e} \\ K_{2i,2j-1}^{e} & K_{2i,2j}^{e} \end{pmatrix} (say) -----(33)$$

We have now obtain from the above Eq.(19)-(33)

$$\begin{split} S^{i,j,e} &= \iint_{Q_e} G^{i,j,e}_{x,y} \ dx \ dy = \iint_{\widehat{Q}} \left(P \ G^{i,j,e}_{u,v} P^T \right) \frac{\partial(x,y)}{\partial(u,v)} \ du \ dv \\ &= 2\Delta_{abc} \ \iint_{\widehat{Q}} \left(P \ G^{i,j,e}_{u,v} P^T \right) \ du \ d \\ &= 2\Delta_{abc} \ P \left(\iint_{\widehat{Q}} \ G^{i,j,e}_{u,v} \ du \ dv \right) \ P^T \\ &= 2\Delta_{abc} \ P \left(K^{i,j,e} \right) \ P^T \qquad -----(34) \end{split}$$

We can thus obtain the global derivative integrals in the physical space or Cartesian space (x,y) by using the matrix triple product established in eqn.(34).

From Eq.(33) and noting the fact that \hat{Q} is the quadrilateral in (u, v) space spanned by the vertices (1/3, 1/3), (0, 1/2), (0, 0)and (1/2, 0) we obtain

$$K^{i,j,e} = \iint_{\widehat{Q}} G_{u,v}^{i,j,e} \, du \, dv$$

=
$$\int_{-1}^{1} \int_{-1}^{1} G_{u,v}^{i,j,e} \, \frac{\partial(u,v)}{\partial(\xi,\eta)} \, d\xi \, d\eta$$
 ------(35)

We now refer to section 5 of this paper, in this section we have derived the necessary relations to integrate the integrals of Eq.(35), As in Eq.(14) and Eq.(15), we use the transformation

$$u(\xi, \eta) = \frac{1}{3}N_{1}(\xi, \eta) + \frac{1}{2}N_{4}(\xi, \eta)$$

$$v(\xi, \eta) = \frac{1}{3}N_{1}(\xi, \eta) + \frac{1}{2}N_{2}(\xi, \eta)$$

to map the quadrilateral $\hat{\Omega}$ to the 2 square $1 \le \xi$ $n \le 1$ Using Eq. (36) in Eq. (35) — we obtain

to map the quadrilateral Q to the 2-square $-1 \le \xi, \eta \le 1$ Using Eq.(36) in Eq.(35), we obtain tripe (f $c^{ij} e^{4+\xi+\eta}$) at a

$$K^{i,j,e} = \iint_{\widehat{0}} G^{i,j,e}_{u,v} \left(\frac{4+\xi+\eta}{96} \right) d\xi d\eta$$
 ------(37)

The submatrices for the quadrilateral Q_e is expressed from Eq.(34) as $S^{i,j,e} = (2\Delta_{abc}) P(K^{i,j,e}) P^{T}$ (38)

In eqn.(38), $2\Delta_{abc} = 2$ x area of the triangle spanning vertices A(x_a,y_a), B(x_b,y_b), C(x_c,y_c) which is scalar.

The matrices P, P^T depend purely on the nodel coordinates (x_a, y_a), (x_b, y_b), (x_c, y_c) the matrix K^{i,j,e} can be explicitly computed by the relations obtained in section 2 and 3. We find that K^{i,j,e} is a (2X2) matrix of integrals whose integrands are rational functions with polynomial numerator and the linear denominator ($4 + \xi + \eta$). Hence these integrals can be explicitly computed. The explicit values of these integrals are expressible in terms of logarithmic constants. We have used symbolic mathematics software of MATLAB to compute the explicit values and their conversion to any number of digits can be obtained by using variable precision arithmetic (vpa) command. The matrix K^e as noted in Eq.(33) is of order ($2xn_{de}$) x ($2xn_{de}$). We have computed K^e for the four noded isoparametric quadrilateral element. This is listed in Table 1A and Table 1B,

7. Application Example :

In this section, we examine the application of the proposed explicit integration scheme to the Saint Venant Torsion problem [22]. Exact solutions for simple cross sections such as circle, ellipse, equilateral triangle and rectangle have been rigorously derived. These problems are described by the following boundary value problem ;

$$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} + 2G\theta = 0 \quad \text{in R}$$

----- (39)

----- (40)

 $\phi = 0$ on ∂R , the boundary of R

where $\phi(x,y)$ is known as Prandtl stress function, G is the shear modulus, θ is the angle of twist per unit length, R is the cross sectional region and ∂R is the boundary of R. We choose $G\theta = 1$ for the sake of simplicity. Then the corresponding torisonal constant is given by the equation

$$t_c = 2 \iint_{P} \phi(x, y) dx dy$$

----- (41)

7.1 Torison of a rectangular Cross section :

We consider the region R as the rectangular cross section with the vertices (-a, b), (a, -b) and (a, b), (-a, b) as shown in Fig.4

From the theory of elasticity [22-24], the Prandtl stress function ϕ and the torisonal constant t_c for the rectangular cross section of length 2b and breadth 2a are given by the following expression in series form



$$\Phi = \frac{32a^2}{\pi^3} \sum_{n=1,3,5,\dots,\dots} \frac{(-1)^{\frac{(n-1)}{2}}}{n^3} \left[1 - \frac{\cosh\left(\frac{n\pi y}{2a}\right)}{\cosh\left(\frac{n\pi b}{2a}\right)} \right] \cos\left(\frac{n\pi x}{2a}\right)$$
(42)
$$t_c = \frac{(2a)^3(2b)}{3} \left[1 - \frac{192}{\pi^5} \sum_{n=1,3,5,\dots,\dots,n} \frac{1}{n^5} \tan\left(\frac{n\pi b}{2a}\right) \right]$$
(43)

These expressions converge rapidly for b > a. In this study we consider the square cross section of unit length for which $a = b = \frac{1}{2}$.

7.2 Finite Element procedure :

We consider the rectunglar region of Fig.4 with $a = b = \frac{1}{2}$. This cross section has four axes of symmetry, therefore, only one eight of the cross section needs to be analysed. We thus have to model the region R, the right isosceles triangular cross section with vertices (0, 0), (1/2, 0), $(1/2, \frac{1}{2})$ as shown in Fig 4. We assume that the domain R is discretised by Quadrilateral elements Q_e , the Prandtl stress function $\phi^e(x, y)$ is expressed in terms of the natural coordinate variates (ξ, η) such that

 $\phi^{e}(x,y) = \sum_{i=1}^{n_{de}} N_{i}^{e}(\xi,\eta) \phi_{i}^{e}$ ------(44)

Where $N_i^e(\xi, \eta)$ denotes the basis function at node i, ϕ_i^e is the corresponding nodal value and n_{de} denots the number of nodes per element. Using the modified Galerkin weighted residual method, the numerical solution of the above boundary value problem for the domain R is expressed as

 $\begin{bmatrix} K \end{bmatrix} \{ \varphi_N \} = \{ F_N \} , \qquad (N = 1, 2, \dots, n_d) \qquad -----(45)$ Where $n_d =$ the numbers of nodes used in discretisation of R. Where $\begin{bmatrix} K \end{bmatrix} = \sum_{e=1}^{n_e} \begin{bmatrix} K_{ij}^e \end{bmatrix} , \quad \{ F_N \} = \sum_{e=1}^{n_e} \{ F_i^e \} \quad (i, j = 1, 2, \dots, n_{de}) \qquad -----(46)$ $K_{i,j}^e = \iint_{Q_e} \left(\frac{\partial N_i^e}{\partial x} \frac{\partial N_j^e}{\partial x} + \frac{\partial N_i^e}{\partial y} \frac{\partial N_j^e}{\partial y} \right) dxdy \qquad ------(47)$ $F_i^e = 2 \iint_{Q_e} N_i^e (\xi, \eta) dxdy \qquad ------(48)$ $\{ (\varphi_N, F_N), \quad N = 1, 2, \dots, n_e \} \qquad -----(49)$ $n_e =$ the number of elements of the domain R

7.3 Discretisation and Finite Element Model :

In designing a finite element model, we shall discretise R , the one octant (a right isosceles triangle) with vertices (0, 0), (1/2, 0) and (1/2, 1/2) into quadrilateral elements as described in section 2 - 4. This discretisation

generates the Jacobian $(4 + \xi + \eta) \times a$ constant for all such quadrilaterals of the domain R, We shall consider the following boundary value problem

$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} + 2 = 0 , \text{ within R}$	(50a)
$\phi = 0$, on side AB	(50b)
$\frac{\partial \phi}{\partial n} = 0$, on sides OA and OB, the lines of symmetry	(50c)

Mesh1: The region R, the right isosceles triangle, is discretised into three quadrilaterals which are obtained by joining the centroid to the midpoint of the sides.

Mesh 2: We discretise R into three triangles by joining the centroid of R to the three vertices of R. Then each of these triangles are divided three quadrilaterals. This discretises R into nine quadrilaterals as explained in section 4.

We then discretise the region R into 2^2 , 3^2 , 4^2 , 5^2 , 6^2 , 7^2 , 8^2 and 9^2 triangles of equal size, each of these triangles are further discretised into three quadrilaterals as explained in section 2-4. This will generate meshes 3-10 with 12,27,48,75,108,147,192 and 243 quadrilateral elements respectively We have depicted these meshes in Figs.5-14. Finite element solutions for these discretisations i.e. for meshes 1-10 is depicted in Tables. 2-12. We find that the numerical solutions converge as the meshes are refined.

In a recent paper[26] a new approach to automatic generation of all quadrilateral mesh for finite analysis is proposed. We have used this to discretised the 1/8-th of the square cross section into

an all quadrilateral mesh. The following MATLAB PROGRAMS are written for this purpose:

(1) D2LaplaceEquationQ4Ex3automeshgen.m

(2)coordinate_rtisoscelestriangle00_h0_hh.m

 $(3) nodaladd resses 4 special_convex_quadrilaterals.m$

(4)quadrilateralmesh_square_cross_section_q4.m

These are appended for reference

Conclusions:

This paper proposes the explicit integration scheme for a unique linear convex quadrilateral which can be obtained from an arbitrary linear triangle by joining the centroid to the midpoints of sides of the triangle. The explicit integration scheme proposed for these unique linear convex quadrilaterals is derived by using the standard transformations in two steps. We first map an arbitrary triangle into a standard right isosceles triangle by using a affine linear transformation from global (x, y) space into a local space (u, v). We discritise this standard right isosceles triangle in (u, v) into three unique linear convex quadrilaterals. We have shown that any unique linear convex quadrilateral in (x, y) space can be mapped into one of the unique quadrilaterals in (u, v) space. We can always map these linear convex quadrilaterals into a 2-aquare in (ξ, η) space by an approximate transformation. Using these two mapping, we have established an integral derivative product relation between the linear convex quadrilaterals in the (x, y) space interior to the arbitrary triangle and the linear convex quadrilaterals of the local space (u, v) interior to the standard right isosceles triangle. Further , we have shown that the product of global derivative integrals $S^{i,j,e}$ in (x, y) space can be expressed as a matrix triple product P (K^{i,j,e}) P^T X (2 * area of the arbitrary triangle in (x, y) space. We have shown that the explicit integration of the product of global derivative integrals in (u, v) space. We have shown that the explicit integration of the product of local derivative integrals in (u, v) space. We have shown that the explicit integration of the product of local derivative integrals in (u, v) space.

partial differential equations. The physical applications of such problems are numerous in science, and engineering, the examples of single equations are the well known Laplace and Poisson equations with suitable boundary conditions and the examples of the system of equations are plane stress, plane stress and axisymmetric stress analysis etc in linear elasticity. We have demonstrated the proposed explicit integration scheme to solve the St. Venant Torsion problem for a square cross section. Monotonic convergence from below is observed with known analytical solutions for the Prandtl stress function and the torisonal constant which are expessed in terms of infinite series as noted in Eqs.(42-43) of this paper. We conclude that an efficient scheme is developed in this paper which will be useful for the solution of many physical problems governed by second order partial differential equations.

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TABLES

 $Table-1A \\ Values of integrals of the product of global derivatives over the quadrilateral {(xk,yk),k=1,2,3,4}={(1/3,1/3),(0,1/2),(0,0),(1/2,0)}, in the interior of the standard triangle (see eqn (33)) IntJdnidnjuvrs=[Ke (2*i-1,2*j-1) Ke (2*i-1,2*j) Ke (2*i,2*j-1) Ke (2*i,2*j)] Ke (2*i,2*j-1) Ke (2*i,2*j)] where, (i,j=1,2,3,4,5,6,7,8) ANALYTICAL VALUES \\ \label{eq:alpha}$

 $\begin{array}{ll} IntJdn1dn1uvrs = [& -11/2-34*log~(2)+27*log~(3), & -1/2-20*log~(2)+27/2*log~(3); ... \\ & -1/2-20*log~(2)+27/2*log~(3), & -11/2-34*log~(2)+27*log~(3) \\ \end{array} \right]$

IntJdn1dn2uvrs = [11/3+68/3*log (2)-18*log (3), 5/6+40/3*log (2)-9*log (3);... 1/3+40/3*log (2)-9*log (3), 25/6+68/3*log (2)-18*log (3)]

IntJdn1dn4uvrs = [25/6+68/3*log (2)-18*log (3), 1/3+40/3*log (2)-9*log (3);... 5/6+40/3*log (2)-9*log (3), 11/3+68/3*log (2)-18*log (3)]

IntJdn2dn1uvrs = [11/3+68/3*log (2)-18*log (3), 1/3+40/3*log (2)-9*log (3);... 5/6+40/3*log (2)-9*log (3), 25/6+68/3*log (2)-18*log (3)]

IntJdn2dn2uvrs = [-22/9-136/9*log (2)+12*log (3), -5/9-80/9*log (2)+6*log (3);... --5/9-80/9*log (2)+6*log (3), -22/9-136/9*log (2)+12*log (3)]

 $\boxed{ IntJdn2dn3uvrs = [14/9+68/9*log (2)-6*log (3), 4/9+40/9*log (2)-3*log (3);... -1/18+40/9*log (2)-3*log (3), 19/18+68/9*log (2)-6*log (3)] }$

IntJdn2dn4uvrs = [-25/9-136/9*log (2)+12*log (3), -2/9-80/9*log (2)+6*log (3);... -2/9-80/9*log (2)+6*log (3), -25/9-136/9*log (2)+12*log (3)]

 $\begin{array}{l} IntJdn3dn2uvrs = [\ 14/9+68/9*log \ (2)-6*log \ (3), -1/18+40/9*log \ (2)-3*log \ (3); ... \\ \ 4/9+40/9*log \ (2)-3*log \ (3), \ 19/18+68/9*log \ (2)-6*log \ (3)] \end{array}$

 $\begin{array}{c} \hline IntJdn3dn4uvrs = [\ 19/18+68/9*\log{(2)}-6*\log{(3)}, \ \ 4/9+40/9*\log{(2)}-3*\log{(3)}; ... \\ -1/18+40/9*\log{(2)}-3*\log{(3)}, \ 14/9+68/9*\log{(2)}-6*\log{(3)}] \end{array}$

 $\begin{array}{l} IntJdn4dn1uvrs = \ [25/6+68/3*\log{(2)}-18*\log{(3)}, \ 5/6+40/3*\log{(2)}-9*\log{(3)}; ... \\ 1/3+40/3*\log{(2)}-9*\log{(3)}, 11/3+68/3*\log{(2)}-18*\log{(3)}] \end{array}$

 $\overline{\text{IntJdn4dn2uvrs}} = -25/9 - \overline{136}/9 * \log (2) + 12 * \log (3), -2/9 - 80/9 * \log (2) + 6 * \log (3); ... -2/9 - 80/9 * \log (2) + 6 * \log (3), -25/9 - 136/9 * \log (2) + 12 * \log (3)$

IntJdn4dn3uvrs = [19/18+68/9*log (2)-6*log (3), -1/18+40/9*log (2)-3*log (3);... 4/9+40/9*log (2)-3*log (3), 14/9+68/9*log (2)-6*log (3)]

 $\begin{array}{l} IntJdn4dn4uvrs = [\ -22/9-136/9*log\ (2)+12*log\ (3), \ \ -5/9-80/9*log\ (2)+6*log\ (3); ... \\ -5/9-80/9*log\ (2)+6*log\ (3), -22/9-136/9*log\ (2)+12*log\ (3)] \end{array}$

Table-1B

Values of integrals of the product of global derivatives over the quadrilateral $\{(xk,yk),k=1,2,3,4\}=\{(1/3,1/3),(0,1/2),(0,0),(1/2,0)\}$, in the interior of the standard triangle (see eqn (33)).

NUMERICAL VALUES IN VARIABLE PRECISION ARITHMETIC

 $\begin{array}{l} \text{intJdn1dn1uvrs} = \text{vpa} \ (\text{sym} ('.595527655000821147485729267330')), \text{vpa} \ (\text{sym} ('.468322285820574645491168269290')); ... \\ \text{vpa} \ (\text{sym} ('.46832228582057464549116826929')), \text{vpa} \ (\text{sym} ('.595527655000821147485729267330')) \ ; \\ \text{intJdn1dn2uvrs} = \text{vpa} \ (\text{sym} (' -.397018436667214098323819511552')), \text{vpa} \ (\text{sym} ('.1877851427862835696725544871395')); ... \\ \text{vpa} \ (\text{sym} (' -.3122148572137164303274455128604')), \text{vpa} \ (\text{sym} ('.102981563332785901676180488448'))) \ ; \\ \text{intJdn1dn3uvrs} = \text{vpa} \ (\text{sym} (' -.3014907816663929508380902442235')), \text{vpa} \ (\text{sym} (' -.3438925713931417848362772435700')); ... \\ \text{vpa} \ (\text{sym} (' -.3438925713931417848362772435700')), \text{vpa} \ (\text{sym} (' -.3014907816663929508380902442235')) \ ; \\ \text{intJdn1dn4uvrs} = \text{vpa} \ (\text{sym} (' \ .102981563332785901676180488448')), \text{vpa} \ (\text{sym} (' -.3122148572137164303274455128604')); ... \\ \text{vpa} \ (\text{sym} (' \ .1877851427862835696725544871395')), \text{vpa} \ (\text{sym} (' -.397018436667214098323819511552')) \ ; \\ \end{array}$

 $\begin{array}{l} \label{eq:sym} (i -.397018436667214098323819511552'), vpa (sym ('-.3122148572137164303274455128604')); ... \\ vpa (sym (' .1877851427862835696725544871395')), vpa (sym (' .102981563332785901676180488448')) ; \\ intJdn2dn2uvrs = vpa (sym (' .264678957778142732215879674369')), vpa (sym (' .1251900951908557131150363247600')); ... \\ vpa (sym (' -.1251900951908557131150363247600')), vpa (sym (' .264678957778142732215879674369')) ; \\ intJdn2dn3uvrs = vpa (sym (' .2009938544442619672253934961491')), vpa (sym (' .2292617142620945232241848290466')); ... \\ vpa (sym (' -.2707382857379054767758151709534')), vpa (sym (' .2099061455557380327746065038509')) ; \\ intJdn2dn4uvrs = vpa (sym (' -.68654375555190601117453658965e-1')), vpa (sym (' .2081432381424776202182970085734')), vpa (sym (' .68654375555190601117453658965e-1')) ; \\ vpa (sym (' .2081432381424776202182970085734')), vpa (sym (' .68654375555190601117453658965e-1')) ; \\ \end{array}{}$

intJdn3dn1uvrs = vpa (sym (' -.3014907816663929508380902442235')), vpa (sym ('-.3438925713931417848362772435700'));...

 $\begin{array}{l} vpa (sym (' -.3438925713931417848362772435700')), vpa (sym (' -.3014907816663929508380902442235')) \ ; \\ intJdn3dn2uvrs = vpa (sym (' .2009938544442619672253934961491')), vpa (sym (' .2707382857379054767758151709534')); ... \\ vpa (sym (' .2292617142620945232241848290466')), vpa (sym (' .2990061455557380327746065038509')) \ ; \\ intJdn3dn3uvrs = vpa (sym (' .3995030727778690163873032519254')), vpa (sym ('.3853691428689527383879075854768')), ... \\ vpa (sym (' .3853691428689527383879075854768')), vpa (sym ('.3995030727778690163873032519254')) \ ; \\ intJdn3dn4uvrs = vpa (sym (' -.2990061455557380327746065038509')), vpa (sym (' .2292617142620945232241848290466')); ... \\ vpa (sym (' -.2707382857379054767758151709534')), vpa (sym ('.2009938544442619672253934961491')) \ ; \\ \end{array}$

Table-2

TORSION OF SQUARE CROSS-SECTION:MESH-1: THREE QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node number	Prand	Prandtl Stress Values		
fem-computed	d values	analytical (theoretical)-values		
5, .779473395549684	5616661049	4884639e-1, .79829131790170537262176536669693e-1		
		·		

Table-3

TORSION OF SQUARE CROSS-SECTION:MESH-2: 9- QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values SHOWN)

node number	Prandtl St	tress Function Values	
fem-compu	ited values	analytical (theoretical)-values	

Table-4

TORSION OF SQUARE CROSS-SECTION:MESH-3: 12- QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node number Prandtl Stress Function Values

fem-computed values analytical (theoretical)-values

 $\overline{16, \ .13029059137868921922272702133360, \ .13010464886468359125466215623221}$

 $17, .79223767223566222816511863813028e-1, .79829131790170537262176536669693e-1\\18, .48150403466555868168471181547365e-1, .48693699564520332429831250748512e-1$

18, .48150405358081084/118154/5058-1, .48095099504520552429851250/485128-1 19, .31242397535836620124969388790690e-1, .32225496081814471416762780958210e-1

Table-5

TORSION OF SQUARE CROSS-SECTION:MESH-4: 27- QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node number Prandtl Stress Function Values

fem-computed values analytical (theoretical)-values

Table-6 TORSION OF SQUARE CROSS-SECTION:MESH-5: 48- QUADRILATERAL ELEMENTS

(ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

noc	node number Prandtl Stress Values			
	fem-com	puted values	anlytical (theoretical)-values	
46,	.143211019	475532824955764	8553650, .14301005788295951	725595268076918
47,	.130137946	923506280698532	9842020, .13010464886468359	125466215623221
48,	.124274412	827598110614776	9009812, .12425010763562328	210221787165997
49,	.99893766015	5774738256159770	195766e-1, .99966331891680868	840902694826967e-1
50,	.86792214881	1356328312243769	271991e-1, .86848158236067333	455652287667199e-1
51,	.48560477985	5656668095881354	604925e-1, .48693699564520332	429831250748513e-1
52,	.26188172918	8558176248811071)81980e-1, .26320778834398639	235310402689663e-1
53,	.113377842	973702079335547	3204885, .11342449829597557	980841251335624
54,	.87739776367	7379138970744541	62629e-1, .87868441821279855	606778663607124e-1
55,	.79718154463	3353022219783879	304410e-1, .79829131790170537	262176536669691e-1
56,	.4321411037	7026819154603624	371216e-1, .43405635618515166	865021126035825e-1
57,	.24277731550	0516451214337020	114154e-1, .24453761494389594	391945108114715e-1
58,	.62771016318	8011897507939300	324700e-1, .62957785243503804	052677732105945e-1
59,	.31954605447	7154489855113085	078633e-1, .32225496081814471	416762780958211e-1
60,	.19670330180	6818827327089734	384029e-1, .19897928847669679	779254406105713e-1
61,	.10796926414	4864615571974859	275303e-1, .11120097424799775	346324124458546e-1

Table-7 TORSION OF SQUARE CROSS-SECTION:MESH-6:75-QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

nod	e number	Prandtl S	Stress Value	s
	fem-compu	ted values	anlytical	(theoretical)-values
—				
67,	.144728160912	2581428265364	72656803,	.14456814738793862691472853858124
68,	.13633685483	8143249310123	63169042,	.13628207221289742574377559202182
69,	.13272853820	0620096789210	09615629,	.13268399708946871663449981516470
70,	.11732519029	0777472416317	13467691,	.11733862929285050890042926192301
71,	.10954983129	8227534842683	02414135,	.10956157070281676867272762921215
72, .	.8607972696010	3685971729556	5272346e-1,	.86135610414287094635657604327851e-1
73, .	7328582731065	51491804709086	6957975e-1,	.73329545131624707159651924771251e-1
74, .	4016630646681	3122647680495	5284043e-1,	.40249054055218616682320834651519e-1
75, .	.2127195474787	4086184277691	176839e-1,	.21359044257827833510365163584636e-1
76,	.12525364046	0181364679534	59767034,	.12524934142062286363549511609375
77,	.10813688326	8284427990267	62651477,	.10818013363726278917382204456608
78,	.10365939057	7227270950859	19037027,	.103698766666427781117751751894623
79, .	7974702042020	4826359705429	509995e-1,	.79829131790170537262176536669693e-1
80, .	.6962440081838	89479438265126	6667743e-1,	.69693083395112164735148953082738e-1
81, .	.3747165222703	4369110805070	0009322e-1,	.37581999150598016943305148301890e-1
82, .	.2030430027586	60357961144324	338020e-1,	.20413616727298556319246302126125e-1
83, .	.9006228431749	0524920926776	6601800e-1,	.90138938192527541739117743928278e-1
84, .	.6714811371638	6073852653925	5039631e-1,	.67262701546232552806716724178216e-1
85, .	.6110793259372	0463260535304	1963036e-1,	.61210310291009902905540140634793e-1
86, .	.3207069777101	2559192141692	2163563e-1,	.32214292180078706690963711081372e-1
87, .	.1806641091204	8367267860827	651059e-1,	.18195828228972691993131269996738e-1
88, .	4645693480124	4082536312624	289246e-1,	.46601374740419173778862258507862e-1
89, .	.2295862250161	2040683735283	8938797e-1,	.23150481555609002594280554851447e-1
90, .	.1415585188331	6966379902332	2665019e-1,	.14316112721877375026405489141045e-1
91, .	7527204620927	5391130589346	6848070e-2,	.77496393243762219590605393381412e-2

Table-8 TORSION OF SQUARE CROSS-SECTION:MESH-7:108-QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node number		Prandtl Stress Values					
	fem-computed	values	anlytical	(theoretical)	-values		
92,	.14554423990634	6970331826	606799007,	.1454151908	37750028202	63415482104	7
93,	.13970765941860	3763041068	06861032,	.1396511012	4150523273	46578917182	4
94,	.13725638608260	2978391728	49967174,	.1372083412	7291368719	53987113547	1
95,	.12663468703175	1699174304	63885978,	.1266254988	3532569572	743325352434	4
96,	.12146658145118	8143067657	95277883,	.1214595412	2022938968	45299309189	5
97,	.10554370074306	4986858755	82831562,	.1055652065	9621227098	81392859528	0
98,	.972421101182083	0345815346	6192466e-1,	.9726009723	6328765263	200055165380)e-1
99,	.752455926839418	0824097666	5683763e-1,	.7528725949	0189508378	116804846224	e-1
100	, .63273294158415	73154215378	80894391e-1	l, .633072067	3842025924	989701270733	32e-1
101	,.34185085985871	8150633890	76840582e-1	,.342410435	6357888141	869840414296	53e-1
102	, .17902909001617	7253181019	03041581e-1	, .179640362	8348059039	325089519859	3e-1
103	, .1318765305820	4768134042	117386174,	.131854610	2158255310	82590070408	73
104	, .1197228690860	3705852902	075076569,	.119732655	2764761819	91960287836	87
105	1168567752160	3804868027	195394189.	.116866015	0568819036	06120724563	81



106, .10002216428157	233658096296087973,	.100058240372051524	90864362009527
107, .9372910778234882	5192044221543913e-1,	.937609766304567869	71846916919905e-1
108, .7154779051479348	6363578759957512e-1,	.716036514449437890	79865602629054e-1
109, .6114220212211994	7126963920609466e-1,	.611896158397585138	42734917399556e-1
110, .3263873268003673	6738637088987260e-1,	.327101845228113141	73416214041160e-1
111, .1734565161445298	8928330606092157e-1,	.174201523757337808	64684142564698e-1
112, .10639651408197	707345502481795394,	.106428225209644136	70159914706797
113, .8931439784044901	3339676976434407e-1,	.893688317088260241	34386380235601e-1
114, .8572274899996617	/0056266475822171e-1,	.857736458472532251	46116320708813e-1
115, .6433557625494938	89159747146679782e-1,	.644093432389971665	04491410470652e-1
116, .5626989253708218	35417177796166702e-1,	.563345160542211437	14776791003322e-1
117, .2961875376017828	31097198630803242e-1,	.297066754019151486	76262816502475e-1
118, .1608520215969717	7590774667478171e-1,	.161699704064434860	43453603567273e-1
119, .7252180787620153	7230321175547094e-1,	.725943645572310692	04583796183556e-1
120, .5287958021669354	0057095031302893e-1,	.529735427438768516	61390213749539e-1
121, .4815796829678200	9552340289040314e-1,	.482436654961421993	68678617585149e-1
122, .2477233577670242	5885835557004824e-1,	.248822095313380243	15770834330267e-1
123, .1397616720525893	31378892818884035e-1,	.140737252126262562	02038391471982e-1
124, .3583082882680239	2205261136139839e-1,	.359433551100165207	47997583332094e-1
125, .1736705094745700	52465349155911403e-1,	.175095831449432486	67659734963090e-1
126, .1071953458043143	34317437792545774e-1,	.108379045764133932	74612847141552e-1
127, .5577610638983220	3814928787138901e-2,	.574009309789832261	34825232072044e-2

Table-9 TORSION OF SQUARE CROSS-SECTION:MESH-8:147-QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node	number	Pranc	Itl Stress Values	
	fem-com	puted values	anlytical (t	heoretical)-values
121,	.1460321	7556430304869	457280055914,	.14592638948386181559691578243499
122,	.1417399	5727024080076	716433762745,	.14168688745104490995867442564200
123,	.1399631	7940054296405	007106541551,	.13991716447668890639130238850990
124,	.1321926	6115967322896	216479830675,	.13217458156484612345766327865011
125,	.1284985	2352620175980	324933619439,	.12848372538079796455836855412330
126,	.1169664	7453410832275	409166541707,	.11697137629490281003259246387914
127,	.1111285	2686991736260	465091545341,	.11113298180522807143982099779576
128,	.954149869	486352083488	5/181/9062/e-1,	.95436333251404062976863898036597e-1
129,	.8/1368522	582960730500.	14/92/18505e-1,	.87154554834900945414015914032371e-1
130,	.000824023	997403703304.	18495916205e-1,	.00/1421/0009409551/5145045100642e-1
131,	.550084014	53/783190993	38416637129e-1,	.55034/244954235/9109/8821080/9906-1
132,	154500408	802981550417	920370882376-1,	.29//096/61100622//2254899/3856386-1
133,	1250260	10945/1/35030	J/8/3//4213e-1,	.154959/915182182005291/40/5401510-1
134,	.1339209	2502529209759 2664202446720	579539424412,	.15589955212252750920891195421900
135,	.1208/94	3004292440/39 3136190357996	529100295555,	.1208/4001508515804144505955/5012
130,	.1240000	2130189237880 4095073977375	028/05001//0,	.1248/0/33989334191934084//100813
13/,	.11240/0	+U83U8280/2/3 =2502(257582(928707958589,	.1124219088/43552599252/09584/49/
130,	.1081085	0209200070000 476000010455	0334/0040990, 17104400310a 1	.1081215/05159258005952195120/12/
139,	.9105/3051	470230019435.	17104409519e-1, 17704644115-1	.9100/00000551//810509108/0522110e-1 940002942052720724/7009120(54274-1
140,	.040000204	030/11323213.	1//94044115e-1, 26100101222a 1	.849093842053/30/240/9981390843/40-1
141,	.043415520	01/005/25100	201001012220-1,	.04301910/12/2303341//404300/234/6-1
142,	.54201/340	5035803023424.	1/3010/08/3e-1,	.542902002999/52555/58202050/2/4/6-1
145,	.20/010101	.3033092923091 004357103354	02/5502/115e-1, 02022020210-1	.200110/100000904199//91304/0/44/01
144,	1167490	00425/195254	209309203196-1,	.151540920082119190050528104525810-1
145,	.110/400	2401039802292	335221003904, 735766476601	.110/39135/0210520430942511555520
140,	1012010	0041094007009 040070059701	011155045165	.103/119342004491/910903///32/390
14/,	.1015010	0400400032701 196159079721	011155245105,	.10152066160096420550755759795272 95067090302639400220946290469040。1
140,	-050205990 707025014	100130070731	222020105558-1, 5706400288201	.050070075020504705270405004060406-1 7082012170017052726217652666070Ac 1
149,	508337305	400414301002.	57004902002e-1, 072660262500-1	.//02/131/901/03/2021/03/000//040-1 5088/503812013286735236031080/070-1
150,	512157521	315042201100	7200020250E-1, 177407508080-1	5126010002506129132007552509510694976-1 512601000250612821810066523340010-1
151,	268074774	588463484730	188524450840-1	26957490392351579082517320901947 ₀₋ 1
152,	1/3200321	026261830650	10032443004C-1, 107884030550-1	1/370507325368081880605650/13710 ₀₋ 1
155,	903123674	760683100677	177004050550-1, 212218118560-1	90350960376336886947737012872892 ₉₋ 1
155	744800389	570286028501	633364806300-1	745332308042124253700773214802650-1
155,	715257410	1031/07270707	222204020020-1, 207322500010-1	7157705703872225517786775214072050-1
157	528264380	530174560264	2)7322370710-1, 20673437133o-1	528895849331490440477885770646480-1
157,	462453341	426726923201	615019703080-1	46301350932017083243007058077734 ₀₋ 1
150,	239877455	535976112329	59999604914e.1	24059233255905805797611268093001e-1
160	130442502	889140043896	177314338760-1	131096569700592847581519114692940-1
161	594919758	440529921253	70706627155e-1	595551913485217999214487676818990-1
162	427349072	675760415616	89907027155C-1,	42811746107054280672305209012921
163	389355116	629275227357	75107871093e-1	39005937190063388467382392661731e-1
164	197530055	8401399909034	15049824638e-1	19840166960456361216923631430329e-1
165	111554480	525463331308	196028448220-1	112298768832915150681122116515030-1
166	285428364	619038620468	17795831728e-1	286319755792912627787748866767356-1
167	136440020	5106850330164	68072487030-1	137548236034881716132181883367650-1
168	.842791726	340962372497	71714736477-2	.851741904786105880755673058443066.2
169	431555611	411563354304	226934428580-2	443816789294761862445611131814900-2
102,	-51555011			.775010/0/2/7/01002445011151014906-2

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Table-10 TORSION OF SQUARE CROSS-SECTION:MESH-9:192-QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node	e number	Prandtl Stress Values	
	fem-com	puted values anlytical (1	theoretical)-values
			,
154.	.14634653	554777987125274240559658.	.14625800572427238855872195713380
155.	.14305825	810033093099901496875320.	.14301005788295951725595268076918
156.	.14170992	085273292060267835568968.	.14166760569746282343907761055730
157	13577708	908440297077607669500441	13575571989496849937124947179516
159	1320000/	1058350132831165028002231	132081803602/366/000611326210531
150,	10405229	278027770215601345121208	124250100500245004500011520215551
127,	11001410	7020252792770252920022	11001172700550404052600154651053
100,	.11991419	//0000000/02//02000009900,	.119911/3/09330494932099134031933
101,	.10810042	0/951/5/05900/1505/55951,	.10811000524559497955702899774480
162,	.10202948	9/202985139/48599466960/,	.10203783794553199515609861763521
163,	.868293812	5/10848/8020/13332310/5e-1,	.8684815823606/33345565228/66/199e-1
164,	.788005042	19526948965346993500049e-1,	.78816293923525654496074837356758e-1
165,	.597985021	76018389466712293453672e-1,	.59823601770331444094709978470898e-1
166,	.495717001	01741499606583680990219e-1,	.49592488018298537801346850337020e-1
167,	.262911270	30041432129754798062572e-1,	.26320778834398639235310402689664e-1
168,	.135905930	76434694148606977762650e-1,	.13623237373811829954185964042501e-1
169,	.13857806	429165344322604744805759,	.13854948115069686535967414175032
170,	.13159231	290514186805028400236985,	.13158085130727430175288314789359
171,	.13011518	878340920136870120552276,	.13010464886468359125466215623221
172,	.12051250	476506369242538983892288,	.12051581611974483038552993377550
173,	.11738180	157774891341903512221519,	.11738509111782797499708781463440
174,	.10495751	313228598566168419038306,	.10497258055491199207030832896719
175,	.999527766	21892208193161915402779e-1,	.99966331891680868840902694826965e-1
176,	.844102565	35585874265788457209208e-1,	.84434317166913011257250880437524e-1
177.	.772728182	58249100866024904942641e-1.	.77293743737041241819601348339065e-1
178.	582250887	38349474425463351200635e-1.	.58255762277003269074116307610788e-1
179.	486674968	53500062101633220293229e-1.	.48693699564520332429831250748513e-1
180	256439209	38979853690340761954860e-1	25680179489915586692002345256768e-1
181	133561958	32879411479871838564330e-1	13395128375523027744433964564116e-1
182	12366672	808011697048653695314896	12366726423053812015025811119718
183	11341248	8615078979218899211714894	11342449829597557980841251335624
18/	11171154	611767250607760556067085	11172317545105040101637015080482
185	989675424	573605873358920710006410-1	989898686787148038403248278293270-1
105,	052051547	0222857008025001888054201	052158770222822/072522060766566480 1
100,	707093030	732203/7707230010000342e-1,	7092012170017052726217652666060201
10/,	720410525	20024000055520055570599e-1, 02594253269769304965525° 1	-//02/151/901/055/2021/05500090958-1 728/042/44045324/20010388802308-1
100,	./38418535	925842555887885948855256-1,	./38094204494333402000103888023980-1
109,	.552209507	100/13230234/5935483011e-1,	.552582208240078250499707804009050-1
190,	.400308183	18381298435200530522009e-1,	.400092//3410839980/2339/9191/4808-1
191,	.244110409	04380935101815259258242e-1,	.24455/01494589594591945108114/156-1
192,	.128380/42	10144669540542/33531844e-1,	.1288094432820580017/6806003764626-1
193,	.10266679	924127930716222146178505,	.10268781507636937406046465859372
194,	.898650254	09659917603614497095178e-1,	.89895330597281725112954778154425e-1
195,	.878393428	16649907147119435741927e-1,	.87868441821279855606778663607123e-1
196,	.727590530	03358681639929106843376e-1,	.72797605570266589097450766540492e-1
197,	.683302278	86473766810272857528888e-1,	.68365607770162579958277184890891e-1
198,	.506178593	81749633725270711157157e-1,	.50662778860007909719826628761236e-1
199,	.433661934	62570470069621126296126e-1,	.43405635618515166865021126035824e-1
200,	.225196897	92552289309141586766232e-1,	.22568560188375041087224792019057e-1
201,	.1200366172	25132241264289702191484e-1,	.12050685583447566463119472402700e-1
202,	.772245072	02129625522450720670336e-1,	.77262510944337357034808439985678e-1
203,	.629111280	61269556092708027681875e-1,	.62957785243503804052677732105948e-1
204,	.604336519	54872659511788083933460e-1,	.60477896465333378649437415184368e-1
205,	.441315098	43718274728090978658638e-1,	.44185301398866359221673132894819e-1
206,	.386547340	85537548644350664727333e-1,	.38702490399152458669802740855107e-1
207,	.198405234	86365493228149122478496e-1,	.19897928847669679779254406105712e-1
208,	.107985579	62446369846744731551803e-1,	.10850583300801482524726020279668e-1
209,	.4967140492	22619140535101479766773e-1,	.49725435093505123305505220987829e-1
210,	.3529624634	42948841350143479983845e-1,	.35359944476345665783263082120396e-1
211.	.321672404	91060174308371186392817e-1.	.32225496081814471416762780958210e-1
212.	.161531739	89818981185225241458735e-1.	.16222362952480223955677393158016e-1
213.	.912903179	11218391561644473232356e-2.	.91878150598037827090979740293448e-2
214.	.233246305	82332958718358743083866e-1.	.23396745960078524057608442063126e-1
215.	.110329327	48901124596240453431315e-1	.11120097424799775346324124458548e-1
216.	.681898308	91300267338440628383479e-2.	.68892199109707352179745513652752e-2
217	.344852073	73789427857946139568814e-2	.35446193557322503151795220028075e-2
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Table-11 TORSION OF SQUARE CROSS-SECTION:MESH-10:243-QUADRILATERAL ELEMENTS (ONLY NONZERO Prandtl Stress Values at the centroid of triangles SHOWN)

node number

Prandtl Stress Values

191, .14662035046283917363880537183069,	.14648559012941637969898953360208
192, .14402110916078072191436650304695,	.14391819240732150678302666792598
193, .14296218306959277748452178422334,	.14286421806373270433042605183193
194, .13828332317405230509548681203758,	.13820181362973855956283284710315
195. 13611643711223459318761663093685.	13603817042923104314037124070908
196 12924980897729028620205496012455	12918338008863611549726099066959
107 1252012226072012020202020202012455,	12592602202605607650862680676045
197, .12509155500789122467829992018290,	.12562095205095097059605060070945
198, .11668120086664601432006310013615,	.11062/3040005/442335896220382281
199, .11202038963255984237527293424377,	.11196806593371102597368642758199
200, .10025817481091249016677791306698,	.10021691297758777459141409021574
201, .94158896233189273375374986921318e-1,	.94119398985631108021510652055242e-1
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261, 11 112 / 501 2 / 705 10 10 10 24427 77 755 / 04C*1, 262 02/101/786027 45782822101211 400 40- 2	01/022230275525060522200220022001706-1
202, .7241014/0002/43/03023181211480488-2,	.717034333041334300934340180198496-2
205, .421499890104/4385153843166287693e-1,	.4210/893805004264641054080135656e-1
264, .29510399820106733300800548920283e-1,	.29/38899225946110653414904377857e-1
265, .27201724850057265371508700307275e-1,	.27108510548354051346499846649297e-1
266, .13477499388549894445555638942295e-1,	.16552101513257453110840999392127e-1
<u>267, .81693388207229677812074387903611e-2, .</u>	.76713270993821192467251305444270e-2

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TABLE-12	
TORISONAL CONSTANT (tc)	
tc=.14057701495515551037840396020329(ANALYTICAL V	ALUE)

FEM MODEL	NO.OF QUADRILATERALS (NO.OF T6-TRIANGLES)* NO OF NODES	fem-computed values of tc
	3(1)*5	.13083989888840093881392607627265
MESH-2	12(4)*19	.13795314846010888055935252663739
MESH-3	27(9)*37	.13941867439787643949762680667990
MESH-4	48(16)*61	.13993063385734349514300036322959
MESH-5	75(25)*91	.14016582079079076182350837373090
MESH-6	108(36)*127	.14029273101444520386658952876026
MESH-7	147(49)*169	.14036885017128652307484475599502
MESH-8	192(64)*217	.14041804850446187732724063014883
MESH-9	243(81)*271	.14053626365883553894393627363271
MESH-10	300(100) *331	0.140475648374825
MESH-11	363 (121)*397	0.14049335294041
MESH-12	432 (144)*469	0.140506793836505
MESH-13	507 (169)* 547	0.14051723770694
MESH-14	588 (196)* 631	0.140525513575901
MESH-15	675 (225)* 721	0.140532182472916
MESH-16	768 (256)* 817	0.140537635039182
MESH-17	867 (289)* 919	0.140542150048631
MESH-18	972 (324)* 1027	0.140545930756678
MESH-19	1083 (361)*1141	0.140549128181663
MESH-20	1200 (400)*1261	0.140551856423775
MESH-25	1875 (625)*1951	0.140560935627972
MESH-30	2700 (900)* 2791	0.140565858672553
MESH-35	3675 (1225)*3781	0.140568823558516
MESH-40	4800 (1600)*4921	0.14057074624724
MESH-45	6075 (2025)*6211	0.140572063602523
MESH-50	7500 (2500)*7651	0.140573005439404

COMPUTER PROGRAMMES

(1)PROGRAM-1

function[]=D2LaplaceEquationQ4Ex3automeshgen(ndiv) syms coord nnel=4; ndof=1; nc=(ndiv/2)^2; nnode=(ndiv+1)*(ndiv+2)/2+nc; nel=3*nc; sdof=nnode*ndof; ff=(zeros(sdof,1));ss=(zeros(sdof,sdof)); format long g for i=1:nel N(i,1)=i; end for i=1:nel NN(i,1)=i; end disp('rr=nodal arrangement over the 1/8th square cross section') [coord,gcoord]=coordinate_rtisoscelestriangle00_h0_hh(ndiv); $[nodetel, nodes] = nodaladdresses 4 special_convex_quadrilaterals(ndiv);$ % %bcdof=[2;5;3] nnn=0; for nn=1:nnode if coord(nn,1)==(1/2) nnn=nnn+1; bcdof(nnn,1)=nn; end end

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bcdof: mm=length(bcdof); format long g k1 =double(0.14057701495515551037840396020329); xi=(zeros(nnode,1)); a0=8/pi^3; for m=1:nnode x=(gcoord(m,1));y=(gcoord(m,2));rr=(0); for n=1:2:99 rr=rr+(-1)^((n-1)/2)*(1-(cosh(n*pi*y)/cosh(n*pi/2)))*cos(n*pi*x)/n^3; end xi(m.1)=(a0*rr): end for L=1:nel for M=1:3 LM=nodetel(L,M); xx(L,M)=gcoord(LM,1); yy(L,M)=gcoord(LM,2); end end % table1=[N nodes]; table2=[N xx yy]; %disp([xx yy]) intJdn1dn1uvrs =[vpa(sym('.595527655000821147485729267330')), vpa(sym('.468322285820574645491168269290'));vpa(sym('. .46832228582057464549116826929')), vpa(sym('.595527655000821147485729267330'))]; intJdn1dn2uvrs =[vpa(sym(' -.397018436667214098323819511552')), vpa(sym('.1877851427862835696725544871395'));vpa(sym(' -.3122148572137164303274455128604')), vpa(sym('.102981563332785901676180488448'))]; intJdn1dn3uvrs =[vpa(sym(' -.3014907816663929508380902442235')),vpa(sym(' -.3438925713931417848362772435700'));vpa(sym(' -.3438925713931417848362772435700')), vpa(sym('-.3014907816663929508380902442235'))]; intJdn1dn4uvrs = [vpa(sym(' -.102981563332785901676180488448')), vpa(sym(' -.3122148572137164303274455128604')); vpa(sym(' -.31221485721371643032785760')); vpa(sym(' -.3122148572137164780'); vpa(sym(' -.3122148572137164780')); vpa(sym(' -.3122148572137164780')); vpa(sym(' -.3122148780')); vpa(sym(' -.31216780')); vpa(sym(' -.3.1877851427862835696725544871395')), vpa(sym('-.397018436667214098323819511552'))]; % intJdn2dn1uvrs = [vpa(sym(' -.397018436667214098323819511552')), vpa(sym(' -.3122148572137164303274455128604')); vpa(sym(' -.3122148572180'); vpa(sym(' -.312214857218604')); vpa(sym(' -.3122148572180')); vpa(sym(' -.31221887160')); vpa(sym(' -.312887160')); vpa(sym(' -.312877160')); vpa(sym(' -..1877851427862835696725544871395')), vpa(sym('.102981563332785901676180488448'))]; intJdn2dn2uvrs =[vpa(sym(' .264678957778142732215879674369')), vpa(sym('-.1251900951908557131150363247600'));vpa(sym(' -.1251900951908557131150363247600')), vpa(sym(' .264678957778142732215879674369'))]; intJdn2dn3uvrs =[vpa(sym(' .2009938544442619672253934961491')), vpa(sym('.2292617142620945232241848290466'));vpa(sym(' -.2707382857379054767758151709534')), vpa(sym('-.2990061455557380327746065038509'))]; intJdn2dn4uvrs =[vpa(sym(' -.68654375555190601117453658965e-1')), vpa(sym('.2081432381424776202182970085734'));vpa(sym(' .2081432381424776202182970085734')), vpa(sym('-.68654375555190601117453658965e-1'))]; % intJdn3dn1uvrs = [vpa(sym('-.3014907816663929508380902442235')), vpa(sym('-.3438925713931417848362772435700')); vpa(sym('-.3438925713930')); vpa(sym('-.3438925713931417848362772435700')); vpa(sym('-.3438925713931417848362772435700')); vpa(sym('-.3438925713931417848362772435700')); vpa(sym('-.343800')); v.3438925713931417848362772435700')),vpa(sym(' -.3014907816663929508380902442235'))]; intJdn3dn2uvrs =[vpa(sym(' .2009938544442619672253934961491')), vpa(sym('.2707382857379054767758151709534'));vpa(sym(' .2292617142620945232241848290466')), vpa(sym('-.2990061455557380327746065038509'))]; intJdn3dn3uvrs =[vpa(sym('.3995030727778690163873032519254')), vpa(sym('.3853691428689527383879075854768'));vpa(sym(' .3853691428689527383879075854768')), vpa(sym('.3995030727778690163873032519254'))]; intJdn3dn4uvrs =[vpa(sym(' -.2990061455557380327746065038509')), vpa(sym(' .2292617142620945232241848290466'));vpa(sym(' -.2707382857379054767758151709534')), vpa(sym('.2009938544442619672253934961491'))]; % intJdn4dn1uvrs = [vpa(sym(' .102981563332785901676180488448')), vpa(sym('.1877851427862835696725544871395')); vpa(sym(' - 102981563332785901676180488448')), vpa(sym(' - 102981563335785901676180488448')), vpa(sym(' - 102981563335785901676180488448')), vpa(sym(' - 102981563335785901676180488448')), vpa(sym(' - 10298156335696725544871395')); vpa(sym(' - 10298156335696725544871395')); vpa(sym(' - 10298156335785901676180'))).3122148572137164303274455128604')), vpa(sym(' -.397018436667214098323819511552'))]; intJdn4dn2uvrs =[vpa(sym(' -.68654375555190601117453658965e-1')), vpa(sym(' .2081432381424776202182970085734'));vpa(sym(' .2081432381424776202182970085734')), vpa(sym('-.68654375555190601117453658965e-1'))]; intJdn4dn3uvrs =[vpa(sym(' -.2990061455557380327746065038509')), vpa(sym(' -.2707382857379054767758151709534'));vpa(sym(' .2292617142620945232241848290466')), vpa(sym('.2009938544442619672253934961491'))]; intJdn4dn4uvrs =[vpa(sym(' .264678957778142732215879674369')), vpa(sym('-.1251900951908557131150363247600'));vpa(sym(' -.1251900951908557131150363247600')), vpa(sym(' .264678957778142732215879674369'))]; % % intJdndn=double([intJdn1dn1uvrs intJdn1dn2uvrs intJdn1dn3uvrs intJdn1dn4uvrs;... intJdn2dn1uvrs intJdn2dn2uvrs intJdn2dn3uvrs intJdn2dn4uvrs;... intJdn3dn1uvrs intJdn3dn2uvrs intJdn3dn3uvrs intJdn3dn4uvrs;... intJdn4dn1uvrs intJdn4dn2uvrs intJdn4dn3uvrs intJdn4dn4uvrs]); % for iel=1:nel index=zeros(nnel*ndof,1); X=xx(iel.1:3): Y=yy(iel,1:3); %disp([X Y]) xa = X(1,1);

xb=X(1,2);

```
xc=X(1,3);
ya=Y(1,1);
yb=Y(1,2);
yc=Y(1,3);
bta=yb-yc;btb=yc-ya;
gma=xc-xb;gmb=xa-xc;
delabc=gmb*bta-gma*btb;
G=[bta btb;gma gmb]/delabc;
GT=[bta gma;btb gmb]/delabc;
Q=GT*G;
sk(1:4,1:4)=(zeros(4,4));SK(1:8,1:8)=(zeros(8,8));
for i=1:4
for j=i:4
sk(i,j)=(delabc*sum(sum(Q.*(intJdndn(2*i-1:2*i,2*j-1:2*j)))));
sk(j,i)=sk(i,j);
end
end
f =[5/144;1/24;7/144;1/24]*(2*delabc);
```

```
%
edof=nnel*ndof;
k=0:
for i=1:nnel
  nd(i,1)=nodes(iel,i);
   start=(nd(i,1)-1)*ndof;
  for j=1:ndof
     k=k+1;
     index(k,1)=start+j;
  end
end
%---
for i=1:edof
  ii=index(i,1);
  ff(ii,1)=ff(ii,1)+f(i,1);
for j=1:edof
  jj=index(j,1);
   ss(ii,jj)=ss(ii,jj)+sk(i,j);
end
end
end%for iel
%----
                                                     .....
%bcdof=[13;37;35;33;31;29;27;25;23;21;19;17;15];
for ii=1:mm
  kk=bcdof(ii,1);
  ss(kk,1:nnode)=zeros(1,nnode);
  ss(1:nnode,kk)=zeros(nnode,1);
  ff(kk,1)=0;
end
for ii=1:mm
  kk=bcdof(ii,1);
  ss(kk,kk)=1;
end
phi=ss\ff;
for I=1:nnode
NN(I,1)=I;
phi_xi(I,1)=phi(I,1)-xi(I,1);
end
MAXPHI_XI=max(abs(phi_xi));
%disp('
                                                                                    _')
%disp('number of nodes,elements & nodes per element')
%[nnode nel nnel ndof]
%disp('element number nodal connectivity for quadrilateral element')
%table1
%disp('
                                                                                                           .)
%disp('element number coordinates of the triangle spanning the quadrilateral element')
%table2
disp('
                           Prandtl Stress Values')
disp(
                                                          anlytical(theoretical)
                                                                                               ')
disp('
                node number
                                  computed values
                                                                                   error
disp(
disp([NN phi xi phi_xi])
disp('
t=0;
for iii=1:nnode
  t=t+phi(iii,1)*ff(iii,1);
end
T=8*t;
```

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')

')

.)

disp(' torisonal constants') disp(' fem=phi exact=xi error=(max(abs(phi_xi))') disp('-------') disp([T k1 MAXPHI_XI]) disp('-------') disp('number of nodes,elements & nodes per element') disp([nnode nel nnel]) disp('------')

(2)PROGRAM-2

```
function[coord,gcoord] = coordinate\_rtisoscelestriangle00\_h0\_hh(n)
%cartesian coordinates ((xi,yi),i=1,2,3) for the right isosceles triangle
% with vertices (x1,y1)=(0,0), (x2,y2)=(1/2,0) and (x3,y3)=(1/2,1/2)
syms ui vi wi xi yi
[ui,vi,wi]=coordinates_stdtriangle(n);
[eln,spqd]=nodaladdresses_special_convex_quadrilaterals(n);
qq=(n+1)*(n+2)/2;
  nc=(n/2)^{2};
for pp=1:nc
qq=qq+1;
q1=eln(pp,1);
q2=eln(pp,2);
q3=eln(pp,3);
ui(qq,1)=(ui(q1,1)+ui(q2,1)+ui(q3,1))/3;
vi(qq,1)=(vi(q1,1)+vi(q2,1)+vi(q3,1))/3;
wi(qq,1)=1-ui(qq,1)-vi(qq,1);
end
%disp([ui vi wi])
N=length(ui);
if N==(n+1)*(n+2)/2+nc
  NN=(1:N)';
for i=1:N
  xi(i,1)=(ui(i,1)+vi(i,1))/2;
  yi(i,1)=vi(i,1)/2;
end
%disp('
                                                               ')
%disp('NN xi yi')
%disp([NN xi yi])
                                                               )
%disp('
else
  disp('ERROR')
end
coord(:,1)=(xi(:,1));
coord(:,2)=(yi(:,1));
gcoord(:,1)=double(xi(:,1));
gcoord(:,2)=double(yi(:,1));
%disp(gcoord)
(3)PROGRAM-3
function[nodetel,nodes]=nodaladdresses4special_convex_quadrilaterals(n)
%eln=6-node triangles with centroid
%spqd=4-node special convex quadrilateral
%n must be even, i.e.n=2,4,6,.....
syms mst_tri x
%disp('vertex nodes of triangle')
elm(1,1)=1;
elm(n+1,1)=2;
elm((n+1)*(n+2)/2,1)=3;
%disp('vertex nodes of triangle')
kk=3:
for k=2:n
  kk=kk+1;
  elm(k,1)=kk;
end
%disp('left edge nodes')
nni=1;
for i=0:(n-2)
  nni=nni+(n-i)+1;
  elm(nni,1)=3*n-i;
end
%disp('right edge nodes')
nni=n+1;
for i=0:(n-2)
  nni=nni+(n-i);
  elm(nni,1)=(n+3)+i;
end
%disp('interior nodes')
```

nni=1;jj=0;

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```
for i=0:(n-3)
  nni=nni+(n-i)+1;
  for j=1:(n-2-i)
    jj=jj+1;
    nnj=nni+j;
    elm(nnj,1)=3*n+jj;
  end
end
%disp(elm)
%disp(length(elm))
jj=0;kk=0;
for j=0:n-1
  jj=j+1;
for k=1:(n+1)-j
  kk=kk+1;
  row_nodes(jj,k)=elm(kk,1);
end
end
row_nodes(n+1,1)=3;
%for jj=(n+1):-1:1
% (row_nodes(jj,:));
%end
%[row_nodes]
rr=row_nodes;
%rr
%disp('element computations')
if rem(n,2)==0
ne=0;N=n+1;
for k=1:2:n-1
N=N-2;
i=k;
for j=1:2:N
  ne=ne+1;
eln(ne,1)=rr(i,j);
eln(ne,2)=rr(i,j+2);
eln(ne,3)=rr(i+2,j);
eln(ne,4)=rr(i,j+1);
eln(ne,5)=rr(i+1,j+1);
eln(ne,6)=rr(i+1,j);
end%i
%me=ne
%N-2
if (N-2)>0
for jj=1:2:N-2
ne=ne+1;
eln(ne,1)=rr(i+2,jj+2);
eln(ne,2)=rr(i+2,jj);
eln(ne,3)=rr(i,jj+2);
eln(ne,4)=rr(i+2,jj+1);;
eln(ne,5)=rr(i+1,jj+1);
eln(ne,6)=rr(i+1,jj+2);
end%jj
end
end%k
end
%ne
%for kk=1:ne
%[eln(kk,1:6)]
%end
%add node numbers for element centroids
nnd=(n+1)*(n+2)/2;
for kkk=1:ne
  nnd=nnd+1;
  eln(kkk,7)=nnd;
end
%for kk=1:ne
%[eln(kk,1:7)]
%end
%to generate special quadrilaterals
\% and the spanning triangle
mm=0;
for iel=1:ne
  for jel=1:3
  mm=mm+1;
    switch jel
     case 1
     nodes(mm,1:4)=[eln(iel,7) eln(iel,6) eln(iel,1) eln(iel,4)];
```



```
nodetel(mm,1:3)=[eln(iel,2) eln(iel,3) eln(iel,1)];
     case 2
     nodes(mm,1:4)=[eln(iel,7) eln(iel,4) eln(iel,2) eln(iel,5)];
     nodetel(mm,1:3)=[eln(iel,3) eln(iel,1) eln(iel,2)];
     case 3
     nodes(mm,1:4)=[eln(iel,7) eln(iel,5) eln(iel,3) eln(iel,6)];
     nodetel(mm,1:3)=[eln(iel,1) eln(iel,2) eln(iel,3)];
    end
   end
end
%for mmm=1:mm
  %spqd(:,1:4)
%end
%
%ss1='number of 6-node triangles with centroid=';
%[p1,q1]=size(eln);
%disp([ss1 num2str(p1)])
%
%eln
%
%ss2='number of 4-node special convex quadrilaterals =';
%[p2,q2]=size(spqd);
%disp([ss2 num2str(p2)])
%
%spqd
(4)PROGRAM-4
function[]=quadrilateralmesh_square_cross_section_q4(nmesh)
%skip=0 or 1
%skip=0,generates meshes for the nodal and coordinate data given for ten cases
%skip=1,generates meshes automatically by dividing sides of triangle into equal sizes of 2,4,6,8,etc.....
clf
skip=1;
for mesh=1:nmesh
    figure(mesh)
  ndiv=mesh*2;
[coord,gcoord]=coordinate_rtisoscelestriangle00_h0_hh(ndiv);
  [nodetel,nodes]=nodaladdresses4special_convex_quadrilaterals(ndiv);
end
[nel,nnel]=size(nodes)
[nnode,dimension]=size(gcoord)
%plot the mesh for the generated data
%x and y coordinates
xcoord(1:nnode,1)=gcoord(1:nnode,1);
ycoord(1:nnode,1)=gcoord(1:nnode,2);
%extract coordinates for each element
for i=1:nel
for j=1:nnel
x(1,j)=xcoord(nodes(i,j),1);
y(1,j)=ycoord(nodes(i,j),1);
end;%j loop
xvec(1,1:5)=[x(1,1),x(1,2),x(1,3),x(1,4),x(1,1)];
yvec(1,1:5)=[y(1,1),y(1,2),y(1,3),y(1,4),y(1,1)];
%axis equal
axis tight
xmin=0;xmax=1/2;ymin=0;ymax=1/2;
axis([xmin,xmax,ymin,ymax]);
plot(xvec,yvec);%plot element
hold on;
%place element number
if mesh<6
midx=mean(xvec(1,1:4));
midy=mean(yvec(1,1:4));
text(midx,midy,['(',num2str(i),')']);
end
end;%i loop
xlabel('x axis')
ylabel('y axis')
st1='one eigth (1/8)square cross section ';
st2=' using ';
st3='bilinear';
st4='quadriateral';
st5=' elements'
title([st1,st2,st3,st4,st5])
text(0.1,0.4,['MESH NO.=',num2str(mesh)])
text(0.1,0.38,['number of elements=',num2str(nel)])
text(0.1,0.36,['number of nodes=',num2str(nnode)])
```

%put node numbers if mesh<6 for jj=1:nnode text(gcoord(jj,1),gcoord(jj,2),['o',num2str(jj)]); end end hold on %axis off end%for nmesh-the number of meshes

FIGURES



one eigth (1/8)square cross section using bilinear quadriateral elements 0.5 0.45 0.4 MESH NO.=2 (12) number of elements=12 **a**10 number of nodes=19 0.35 o19 (10) (11) 0.3 0.25 a XIX 8 0.2 (8) (7) **6**18 0.15 (3) (6) 012 014 (9) 0.1 (1) (4) 0.05 (2) (5) 00 0.5 0.05 0.1 0.15 0.2 0.25 0.3 0.35 0.4 0.45 x axis









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